

NASA Proof-of-Concept 1-W Stirling Convertor Development for Small RPS

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Why Low Power RPS?

Small nuclear power systems that would provide electricity to probes, landers, rovers, or communication repeaters for space missions

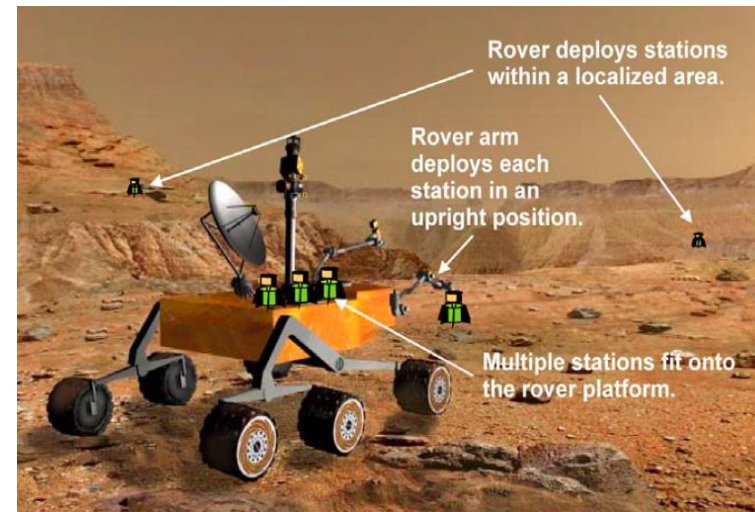
- Operate in vacuum or on planetary surface (ie. Moon, Mars, more...)
- Use conversion technology to convert heat to electricity for powering spacecraft sensors and communications
 - Fractional GPHS (General Purpose Heat Source) offers around 60 watts of thermal input
 - LWRHU (Light Weight Radioisotope Heater Unit, often called RHU) offers around 1 watt of thermal input for each unit and multiple units could be used

Development Goals

- Sufficient power for spacecraft functions
- Long-life and low degradation to ensure power at EOM
- Robust to critical environments (vibration, shock, constant acceleration, radiation)
- Thermal capability and high efficiency

Dynamic Power Conversion

- **12-16% overall system efficiency possible from 1 to 10 watts electrical power output**



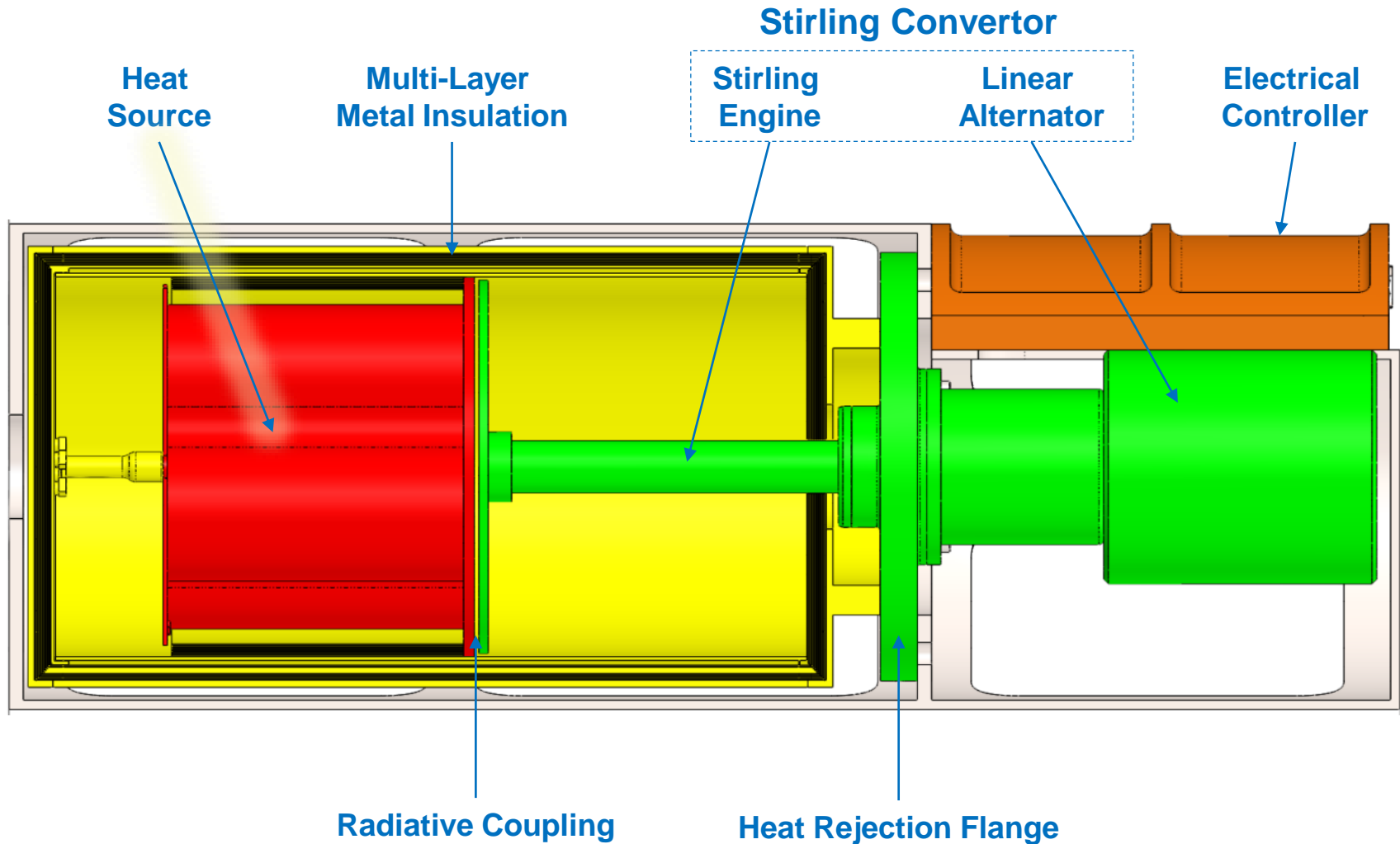
[Ref 1] Conceptualization of Seismic Monitoring Stations Being Deployed from Rover [JPL Pub 04-10, Sept-2004]

Low Power Dynamic RPS Concept

Design Goals

- Long life design (no wear mechanisms)
- 3 kg system mass
- Envelope of 11 cm diameter X 32 cm length
- Performance
 - Heat from multiple LWRHU
 - At least 1 We power output
 - At least 12% system efficiency
 - Maximum of 400 °C acceptor temperature
 - Maximum of 50 °C rejection temperature
- Robustness
 - Overstroke collision tolerant (limited time)
 - Operates in vacuum or atmosphere
 - Launch vibration
 - Constant accelerations
 - Shock
- Compliance
 - Minimize exported force
 - EMI

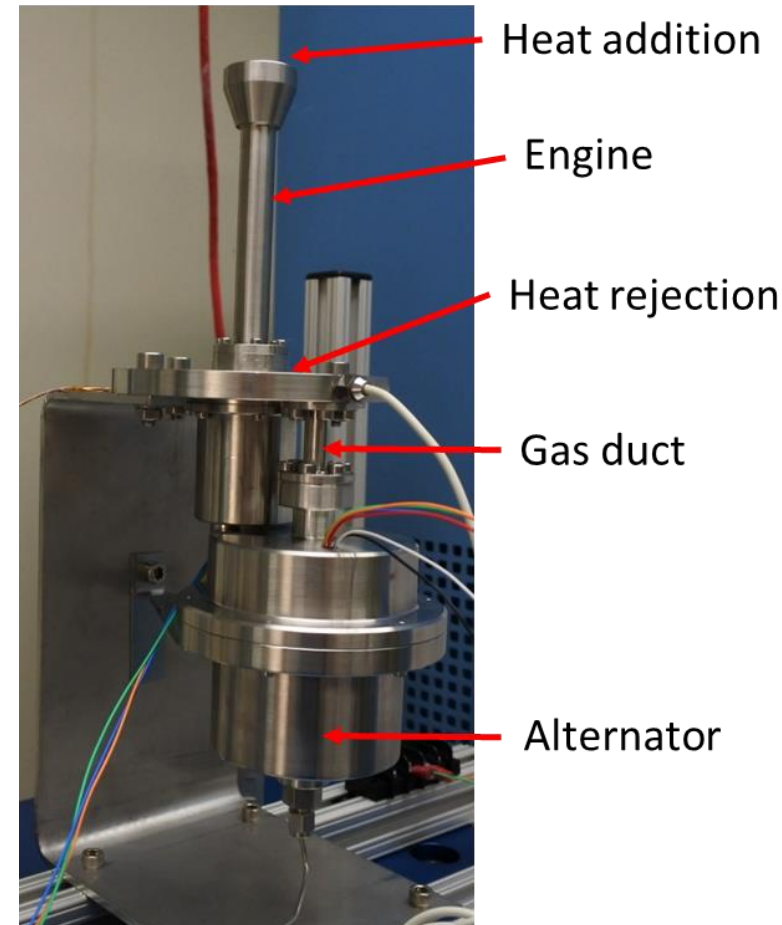
Low Power Dynamic RPS Concept



Stirling Convertor

Proof of Concept – 1 W_e design

- Split-Stirling, gas duct between engine and alternator compression space
- Gap regenerator – no porous matrix
- Flexure bearings for piston and displacer
- Laboratory design did not minimize mass
- Simulating heat from 8x RHUs using electric heater, 350 °C hot end temp
- Fluid loop heat rejection, 50 °C cold end
- 100 Hz, 94 psig helium, 4.0 mm X_p, 2mm X_d

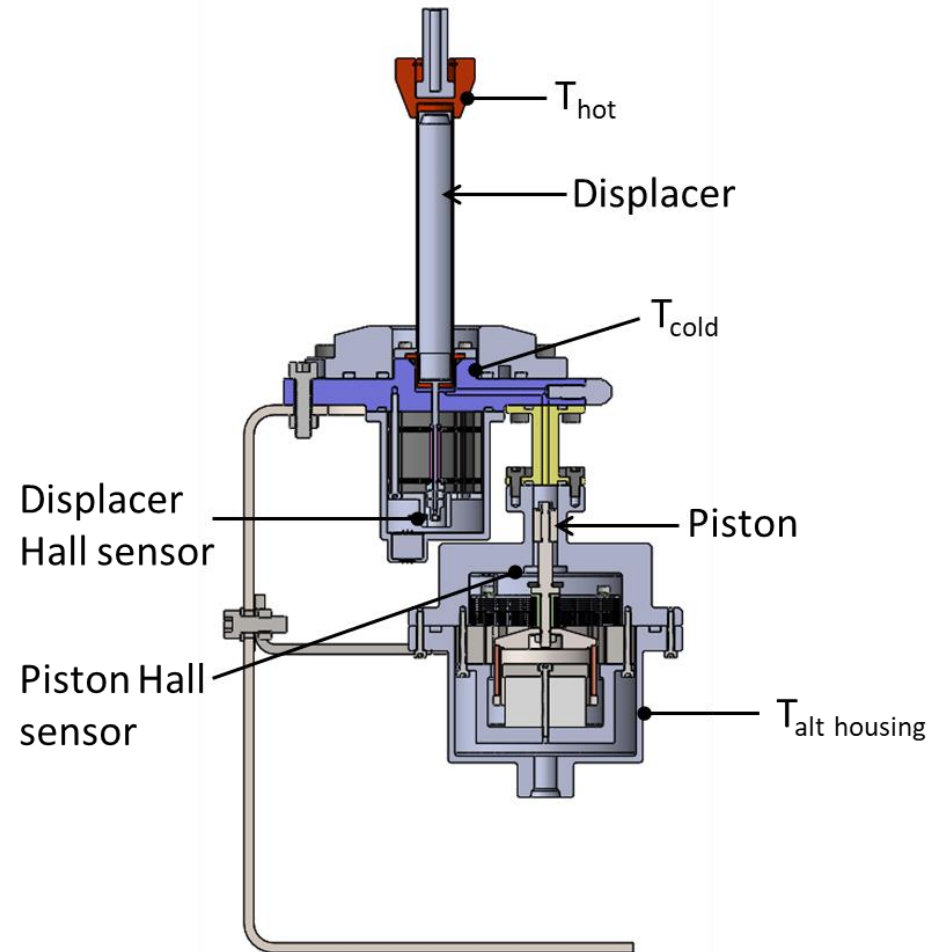


Test Setup
(insulation not shown)

Convertor Instrumentation

Instrumentation

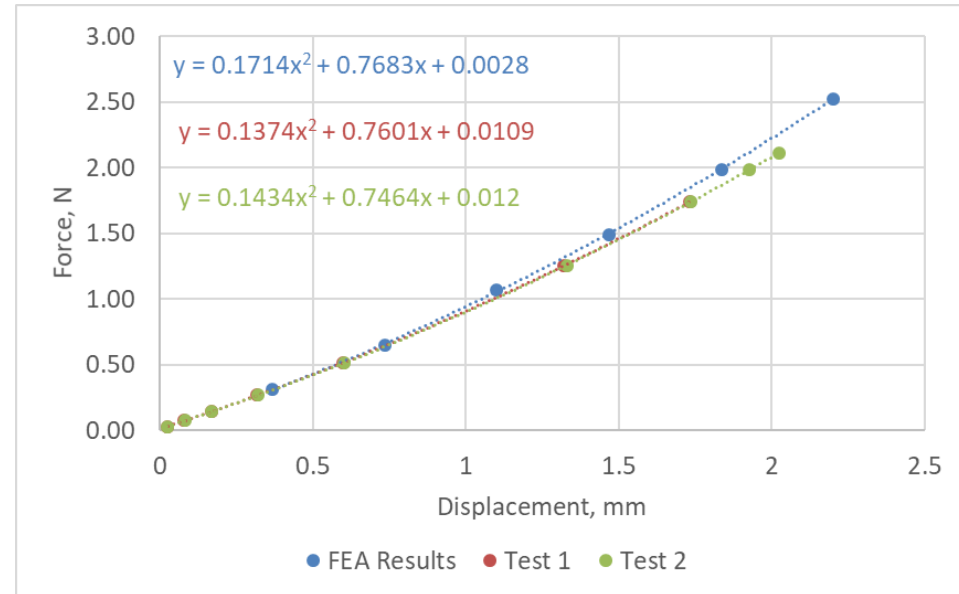
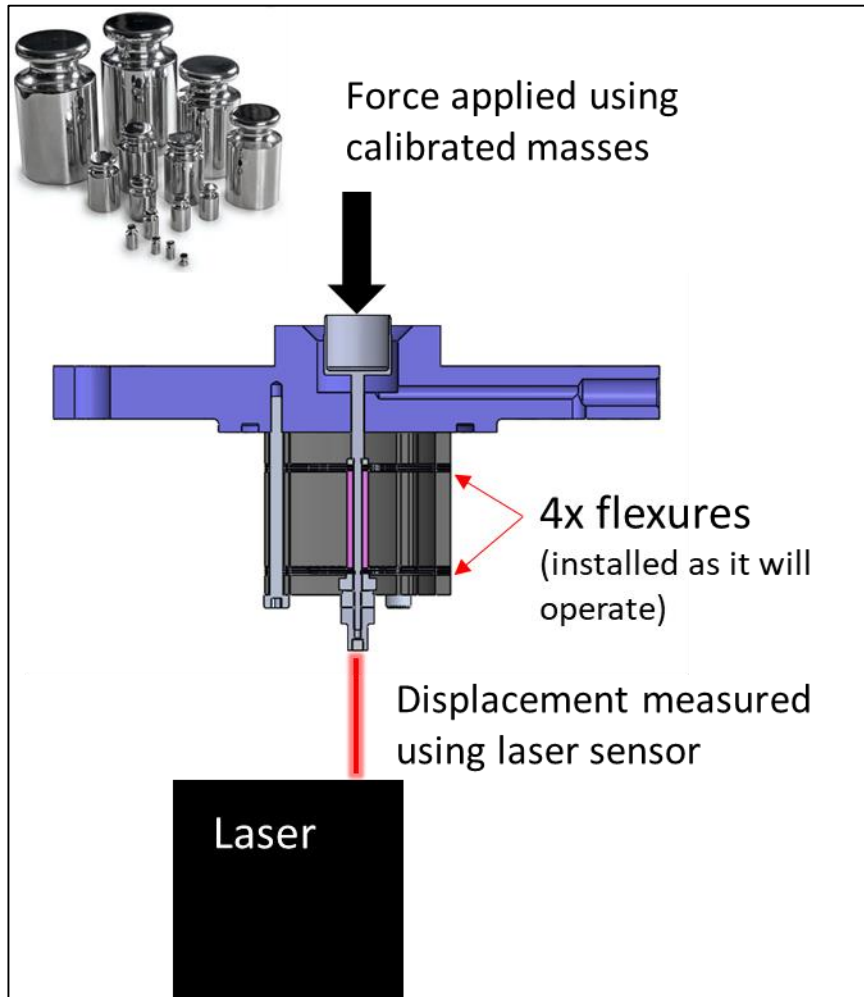
- Piston hall effect sensor
- Displacer hall effect sensors
- Dynamic CS pressure transducer
- Hot end temperature (1x)
- Cold end temperature (1x)
- Alternator housing temperature (1x)
- Electrical heat input
- Alternator output



Testing Sequence

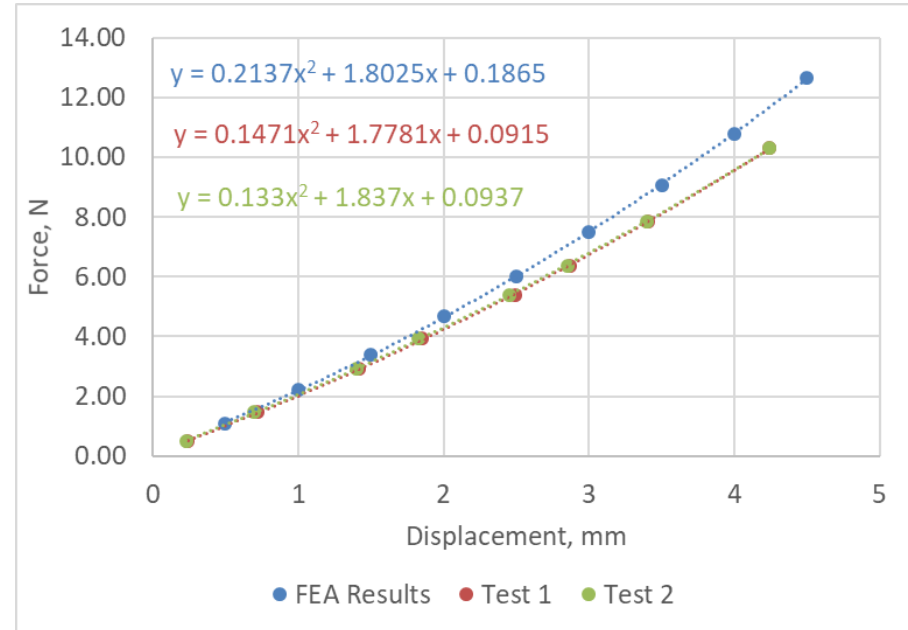
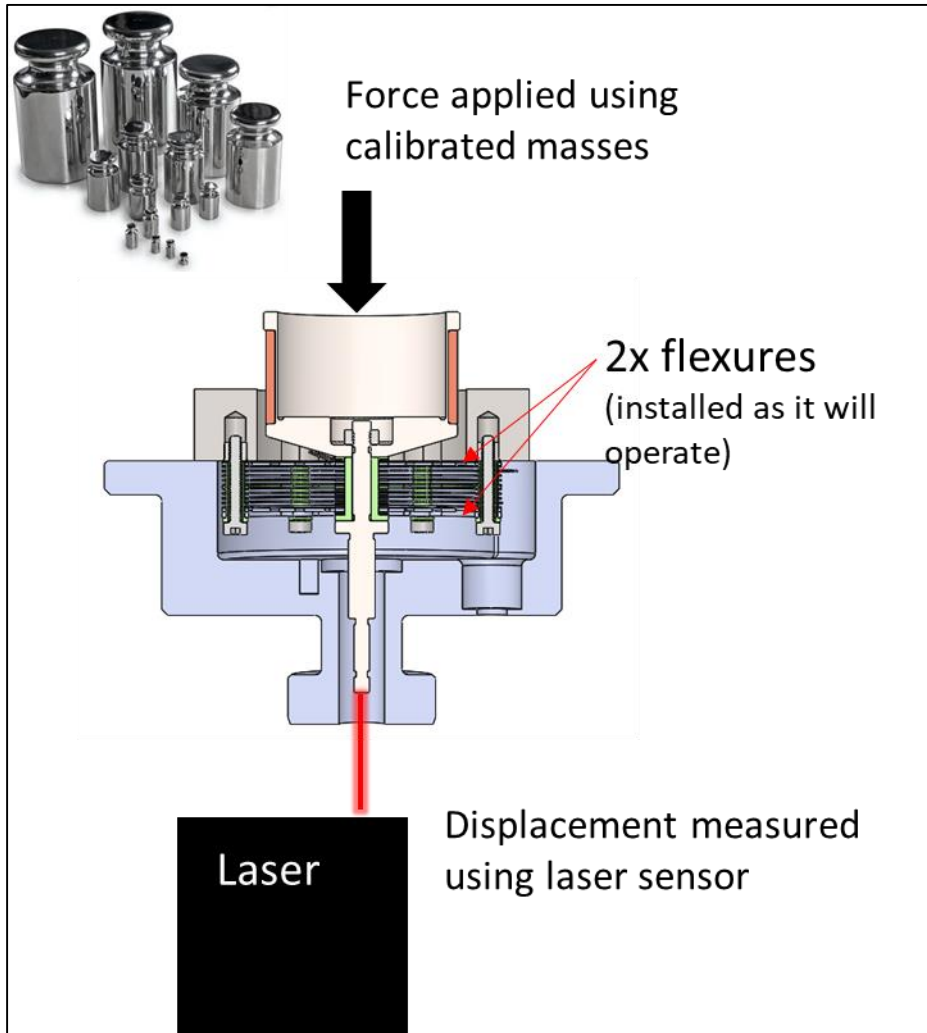
- Flexure Stiffness Characterization
- Displacer & Piston Resonance Characterization
- Displacer & Piston Position Sensor Calibration
- Convertor Characterization

Displacer Flexure Stiffness Characterization



Finite element model over predicted displacer flexure stiffness by 7% at full 2 mm amplitude

Piston Flexure Stiffness Characterization



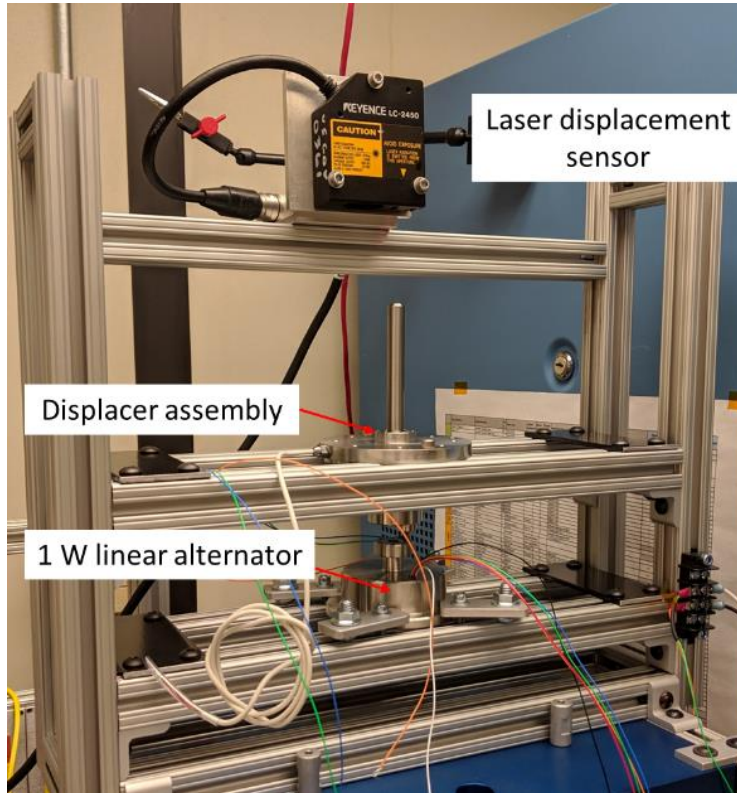
Finite element model over predicted piston flexure stiffness by 13% at full 4 mm amplitude

Displacer Resonance Characterization

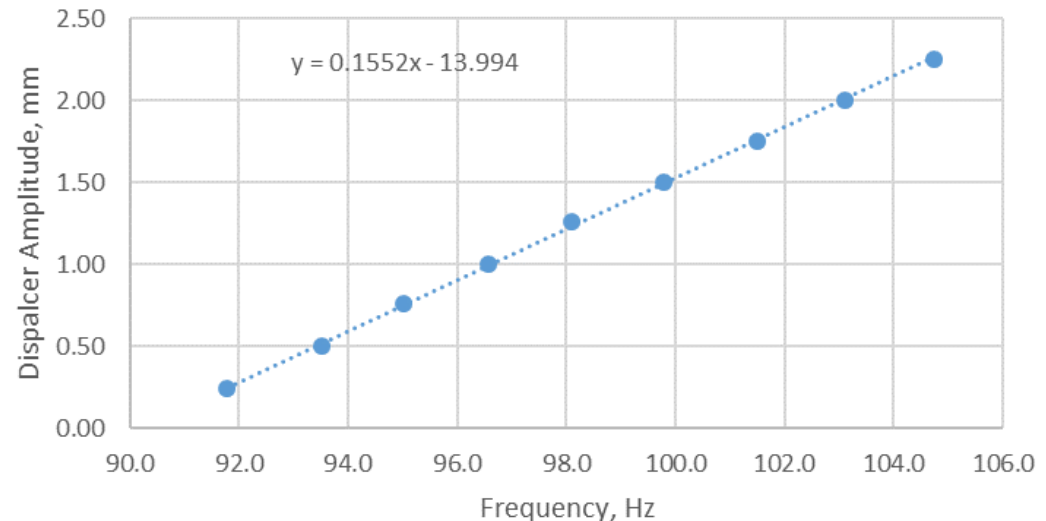
Goal: Achieve 102-103 Hz at 2 mm amplitude

Procedure:

- 1 W linear alternator was used as an exciter driven by an AC source
- Frequency swept from 90 to 104.75 Hz
- Displacer (mass-spring) assembly allowed to resonate
- Adjust number of flexures and mass as needed.



Test setup used for characterizing displacer resonance.



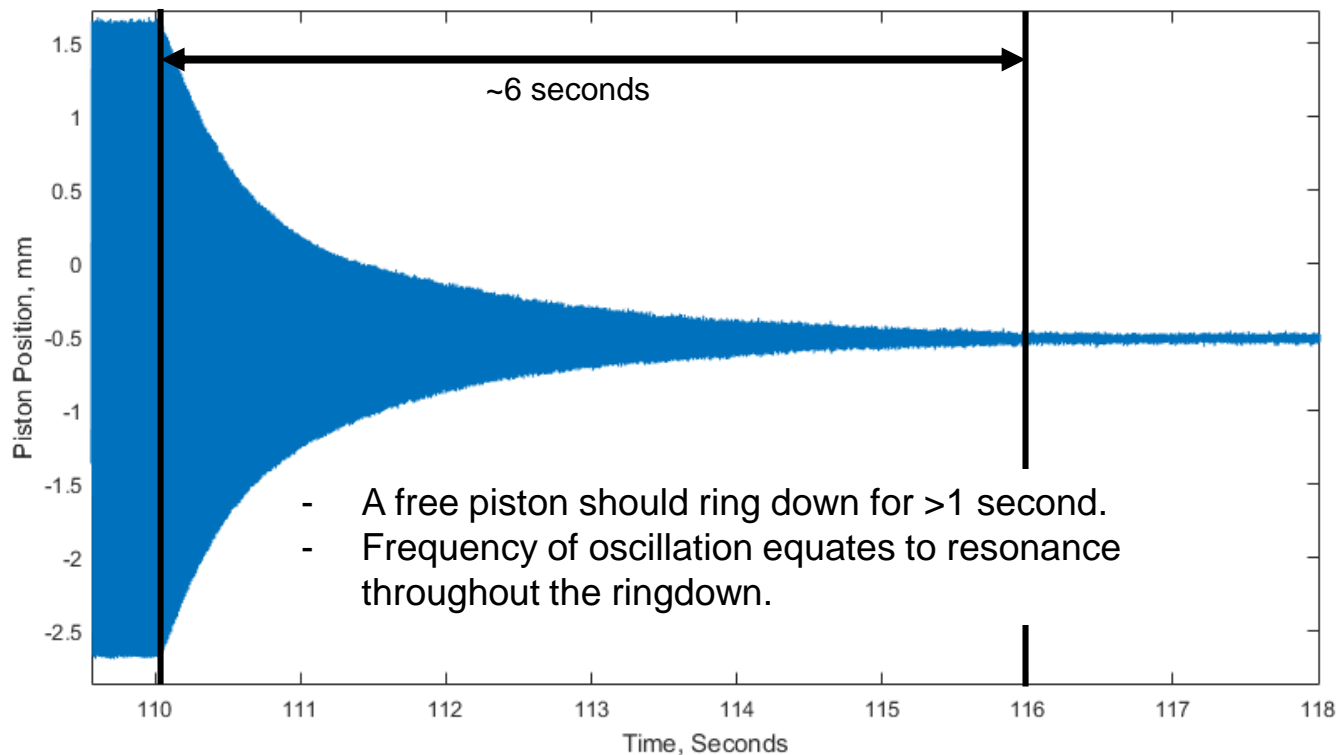
Displacer amplitude (X_d) versus frequency.

Piston Resonance Characterization

Goal: Achieve 95-98 Hz at 4 mm amplitude.

Two Approaches:

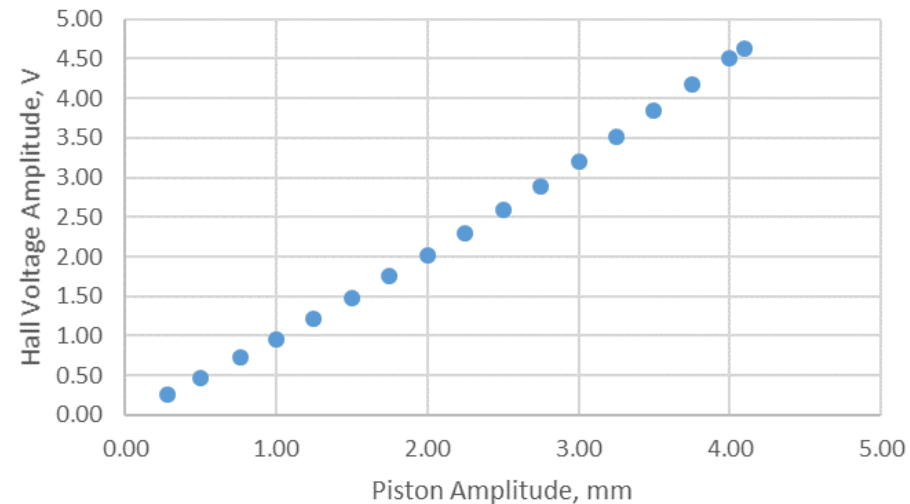
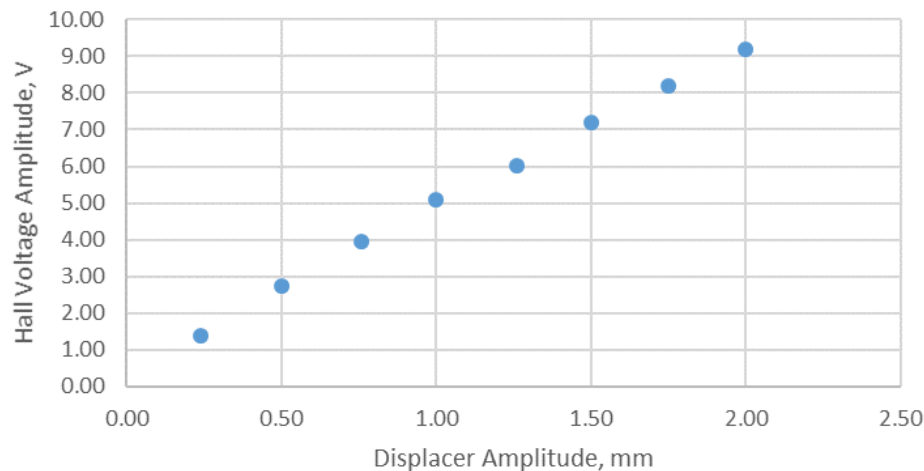
- Resonant approach (used for displacer), requires 2x alternators
- Ringdown
 - Drive alternator to 4 mm, go open circuit on the alternator.



Displacer & Piston Position Sensor Characterization

Procedure:

- Displacer was excited via harmonic resonance.
- 1 W linear alternator was driven via AC source.
- A laser displacement sensor was used to measure position.
- All signals were recorded and monitored via LabVIEW.
- Correlations of hall sensor voltage amplitude to laser amplitude (in mm) were derived.



Signals are linear over and beyond entire operating range.

Convertor Characterization

Test process:

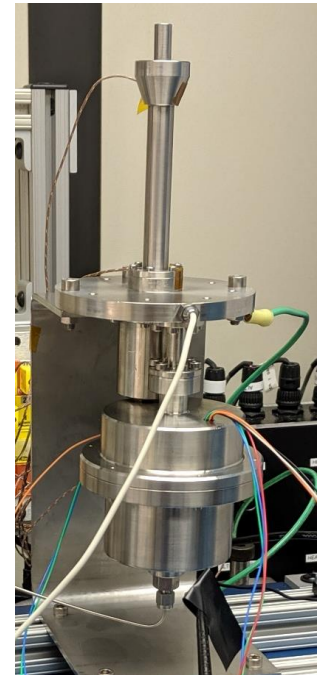
- Engine and alternator assemblies were integrated
- Convertor filled with helium
- Used and AC source to drive the piston
- Motor at piston amplitude of 2 mm at frequencies of 95-103 Hz
- Motor at piston amplitude of 4 mm at frequencies of 95-103 Hz

Observations:

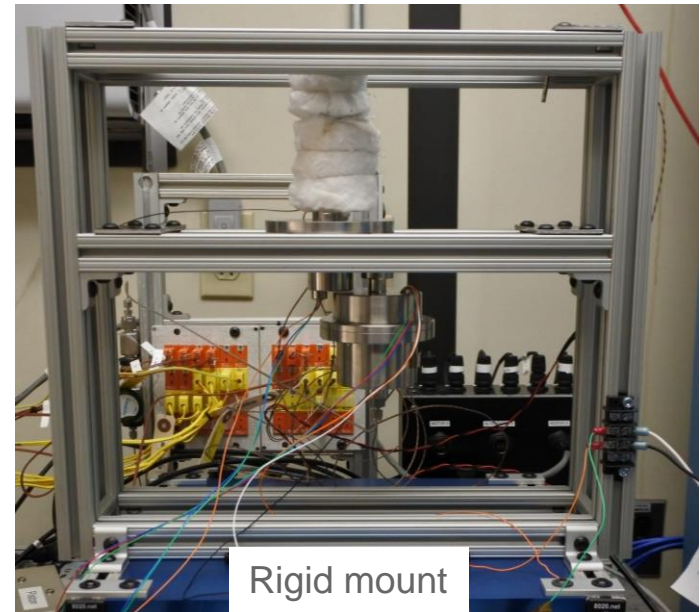
- Round 1 of testing w/ **non-rigid mount**

| | Mode 1 | Mode 2 |
|-------------------|----------|---------|
| Hot-end | Heating | Cooling |
| Xp-Xd Phase Angle | ~170 deg | ~0 deg |

- Measured case motion: 0.1 mm
- Round 2 of testing w/ **rigid mount**
 - Displacer leads piston by 50-80 degrees at frequencies of 95-99 Hz.
 - Cooling of hot-end observed
 - 3.5 W to drive the cooler (rub discovered)



Non-rigid mount



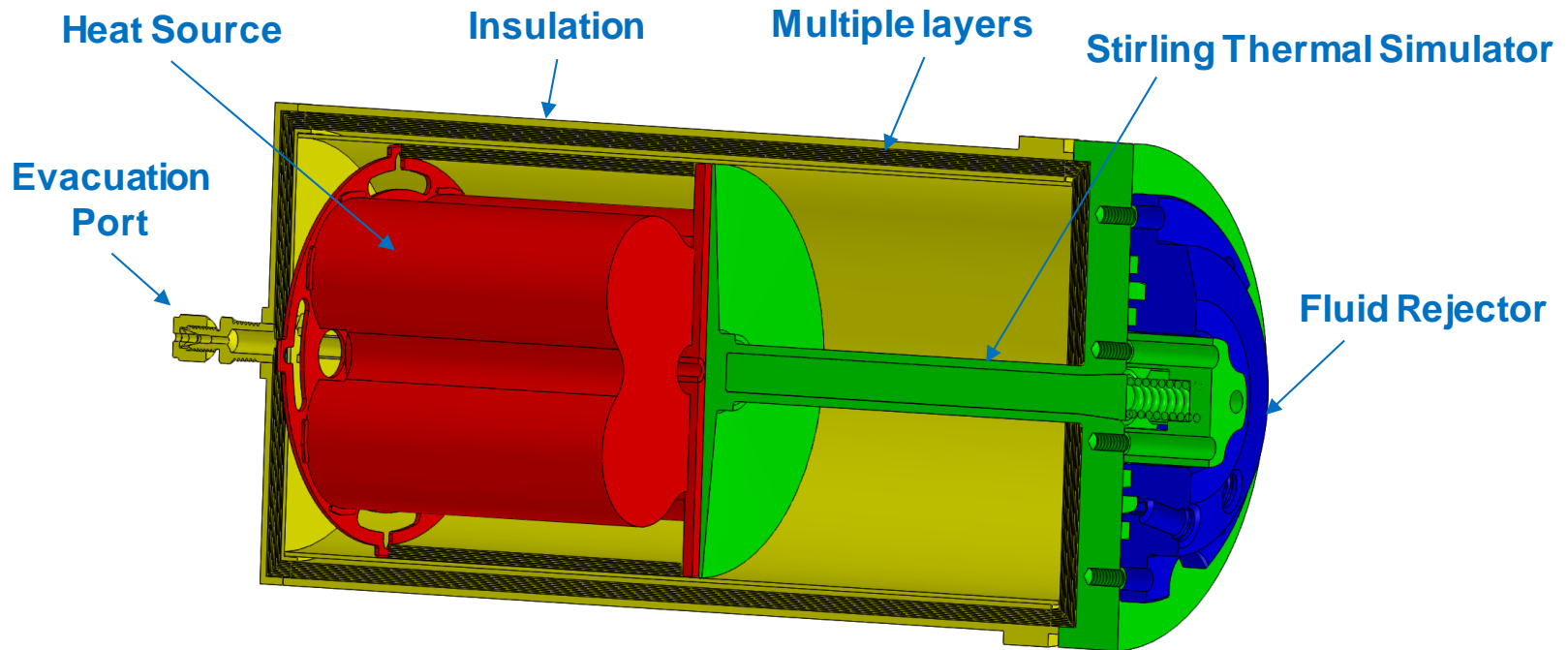
Rigid mount

Insulation – Functional Test

Objective: High performance required (~ 0.001 W/m-K effective thermal conductivity)

- Peregrine Falcon Corp. designed and fabricated multi-layered metal insulation (MLMI)
- The prototype is currently under test at GRC.

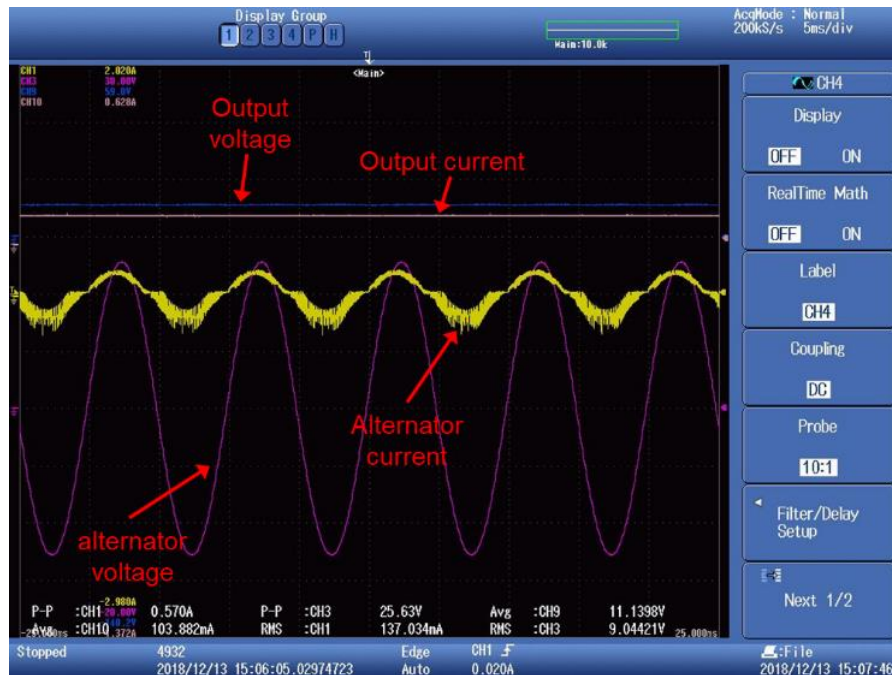
Current Challenge: Low conductance of the evacuation port requires long evacuation time.



Controller

Controller design and functionality

- Linear AC regulator controller using a MOSFET H-bridge with analog circuit to control FETs for AC to DC rectification and load control
- Constant power load monitoring allows for load control and shunting of unused power

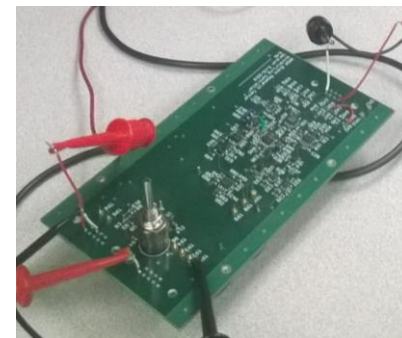


Design Progression

- LTspice model contains a linear alternator, H-bridge rectifier, constant power circuit, and waveform smoothing circuit for power factor and Total Harmonic Distortion correction
- Model validated with breadboard testing.
- Design finalized and incorporated into a printed circuit board design. Assembly in progress

Controller Breadboard Testing Results

| | |
|-------------------------------|------|
| Alternator Voltage, V_{p-p} | 25.6 |
| Alternator Power, W_e | 1.24 |
| Controller Voltage, V_{dc} | 11.1 |
| Controller Power, W_e | 1.16 |
| AC-DC Conversion Efficiency | 93% |



Summary

- Small RPS are being considered for small spacecraft missions
 - Enables long-life power for use in darkness
- 1-W Stirling RPS is in development at NASA GRC
- Testing & Demonstration of Subcomponents is Underway:
 - Convertor
 - High-performance insulation
 - Controller



Special thanks to contributors

- Barry Penswick
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Thank you for attending